

HIGHLY COMPACT DRIVING WEDGE TYPE COUPLING

ENGLISH

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AREAS OF APPL

Product s Which co which pu

TECHNICAL DATA

Product application: Which feature for which coupling Page 07

SERVICE

Explanation of the technical data Page APP-1

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CENTAFLEX-T AT A GLANCE

Torsionally stiff wedge type coupling for high torques in confined spaces.

Based on a bridge bearing principle allowing a high power density and good misalignment properties. Torsionally stiff design, however, highly flexible in axial and angular directions ensuring reliable compensation of misalignments. Proves superior when compared to standard wedge type solutions by an extremely compact design and high performance density achieved by optimising its geometry and benefitial omission of the hubstar.

Also available as homokinetic drive shaft. Easy and safe integration into the drive train.

Features

High flexiblity in design extremely compact build High torsional and radial stiffness Cardanically flexible and resiliant axially low maintenance

Areas of Application



Torque range 1.2 to 24 kNm

Temperature range

 -40° up to $+90^{\circ}$ C (temporary)

For efficient torque transmission and long lifespans at a maximum design flexibility.

CENTAFLEX-T SYSTEM



and offers very high torsional stiffness and power density.

operation in confined spaces.



The CENTAFLEX-T coupling is compensation of misalignments standard series. Its modular diate sizes and multifaceted used as a flexible gear box output special designs.

> Ensuring fast and efficient deriving of customized solutions.

By dispensing special tools and enabling axial as well as radial installation of the couplings, work and the number of parts

Ensuring fast and time-saving mounting of the coupling without need for hubstars or toothing.

When the going gets tough, quality is priceless. With an exemplary Quality Management, CENTA enthe sum of their parts. CENTA entertains the vision of intelligent requirements in terms of design and quality.

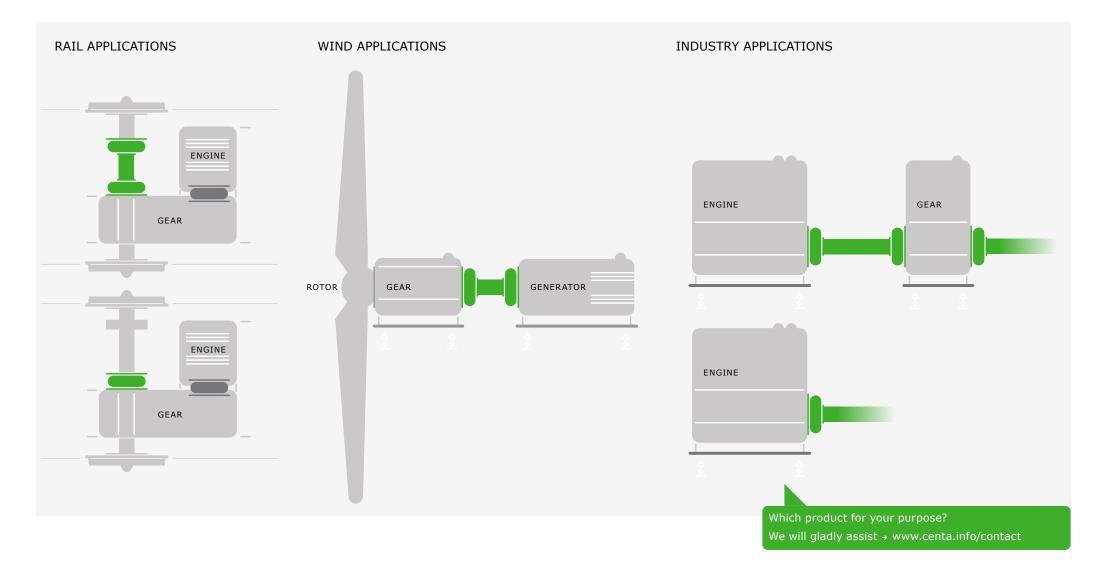


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APPLICATIONS



CENTAFLEX-T APPLICATIONS



TECHNICAL DATA

Questions on product selection?

We will gladly assist \rightarrow www.centa.info/contact





TECHNICAL DATA		↓ SIZES 360-550											
1	2	3	4	5	7	8	9	10	11	12	13	14	15
Size	Rubber quality	Nominal torque	Maximum tor- que	Continuous vibratory torque	Dynamic tor- sional stiffness	Relative dam- Speed ping		Permissible axial displacement	Axial stiffness	Permissible radial displacement	Radial stiffness	Permissible angular displacement	Angular stiffness
	[Shore A]	Τκν	Тктах	Ткw	CTdyn	Ψ	n _{max}	ΔKa	Ca	ΔKr	Cr	ΔKw	Cw
		[kNm]	[kNm]	[kNm]	[kNm/rad]		[min⁻¹]	[mm]	[kN/mm]	[mm]	[kN/mm]	[°]	[kNm/°]
360S	70	5,5	16,5	2,2	400	0,82	2100	2100 ±4	0,90*	±1	9*	±1,5	0,180*
5003	80	6,5	19,5	2,6	564	0,73	2100		1,47*		15*	-1,5	0,295*
360	70	7,5	30	3	2050	1,05	2100	±4	2,10	±1	21	±1,6	0,60
460	70	17	68	6,8	3600	1,05	1650	±6	2,60	±1	36	±1,5	1,00
FFO	70	24	96	9,6	4010,3	1,08	1 500		2,30		27	11.2	1,32
550	80	30	120	12	7700,0	1,06	1500	±5	3,50	±1	35	±1,3	3,10

* preliminary values.

EXPLANATION OF THE TECHNICAL DATA

This appendix shows all explanations of the technical data for all CENTA products.

the green marked explanations are relevant for this catalog:

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5	Continuous vibratory torque	Page APP-2
	Permissible power loss	Page APP-2
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15	Angular stiffness	Page APP-4

Are these technical explanations up to date? click here for an update check!

EXPLANATION OF THE TECHNICAL DATA

1	2		4	5	6	
Size	Rubber quality	Maximum torque		Continuous vibratory torque	Permissible Power Loss	
	Shore A		[kNm]	Tĸw [kNm]	Ркv [kW]	
This spontaneously selected figure des- gnates the size of the coupling.	This figure indicates the nominal shore hardness of the elastic element. The nominal value and the effective val-	Tĸmax	This is the torque that may occur occasionally and for a short period up to 1.000 times and may not lead to a substantial temperature rise in the rubber element.	Amplitude of the continuously permissible periodic torque fluctuation with a basic load up to the value T_{KN} .	Damping of vibrations and displacement results in power loss within the rubber element.	
	ue may deviate within given tolerance ranges.			The frequency of the amplitude has no influence on the permissible continuous vibratory torque. Its main influence on	The permissible power loss is the maxi- mum heat (converted damping work into heat), which the rubber element	
	3 Nominal torque	In addition the following maximum tor- ques may occur:		the coupling temperature is taken into consideration in the calculation of the power loss.	can dissipate continuously to the envi- ronment (i.e. without time limit) with- out the maximum permissible tempera-	
	T _{KN} [kNm] Average torque which can be transmit-	$\Delta T_{\rm Kmax} = 1,8 \times T_{\rm KN}$	Peak torque range (peak to peak) between maximum and minimum torque, e.g. switch-	Operating torque T _{Bmax} [kNm]	ture being exceeded. The given permissible power loss refers to an ambient temperature of 30° C.	
	ted continuously over the entire speed range.	1,071	ing operation. Temporary peak torque (e.g.	The maximum operating torque results of T_{KN} and T_{KW} .	If the coupling is to be operated at a higher ambient temperature, the tem-	
		T _{Kmax1} = 1,5×T _{KN}	ΔTkmax or Tkmax1 may occur 50.000 times alternating or 100.000 times swelling.		perature factor StEREV has to be taken into consideration in the calculation. The coupling can momentarily with- stand an increase of the permissible power loss for a short period under cer-	
		T _{Kmax2} = 4,5хТкм	Transient torque rating for very rare, extraordinary con- ditions (e.g. short circuits).		tain operation modes (e.g. misfiring).	

For a maximum period of 30 minutes the double power loss P_{KV30} is permissible. CENTA keeps record of exact parameters for further operation modes.

St PKV

70

80

90 °C

1,0

0,8

0,6

0,4

0,2

0

20

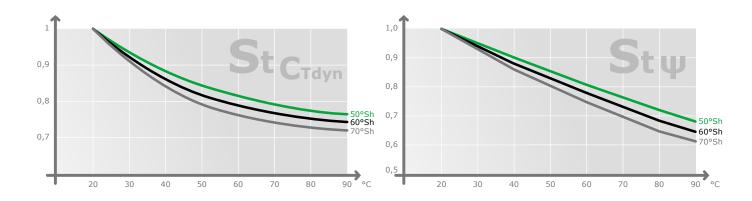
30

40

50

60

EXPLANATION OF THE TECHNICAL DATA



7	8	9	10		
Dynamic torsional stiffness	Relative damping	Speed	Permissible axial displacement		
CTdyn [kNm/rad]	Ψ	[min ⁻¹]	[mm]		
The dynamic torsional stiffness is the relation of the torque to the torsional angle under dynamic loading. The torsional stiffness may be linear or progressive depending on the coupling design and material. The value given for couplings with linear torsional stiffness considers following terms: • Pre-load: 50% of TKN	The relative damping is the relationship of the damping work to the elastic de- formation during a cycle of vibration. The larger this value $[\psi]$, the lower is the increase of the continuous vibratory torque within or close to resonance.	The maximum speed of the cou- pling element, which may occur occasionally and for a short pe- riod (e.g. overspeed). The characteristics of mounted parts may require a reduction of	 The continuous permissible axial displacement of the coupling. ΔK_a This is the sum of displacement by assembly as well as static and dynamic displacements during operation. 		
 Amplitude of vibratory torque: 25% of T_{KN} Ambient temperature: 20°C Frequency: 10 Hz 	The tolerance of the relative damping is ±20%, if not otherwise stated. The relative damping is reduced at higher temperatures.	the maximum speed (e.g. outer diameter or material of brake discs). The maximum permissible	The maximum axial displace- ment of the coupling, which may occur occasionally for a short period (e.g. extreme load).		
For couplings with progressive torsional stiffness only the pre-load value changes as stated. The tolerance of the torsional stiffness is $\pm 15\%$ if not stated otherwise.	Temperature factor $S_{t^{\Psi}}$ has to be taken into consideration in the calculation. The vibration amplitude and frequency only have marginal effect on the rela- tive damping.	nd speed of highly flexible cou- pling elements is normally 90% thereof.	ΔK _{a max} The concurrent occurrence of different kinds of displacements is handled in technical documents (displacement diagrams, data sheets, assembly instructions)		
The following influences need to be considered if the torsional stiffness is required for			tions).		

other operating modes: • Temperature

Higher temperature reduces the dynamic torsional stiffness.

Temperature factor $S_t\,c_{Tdyn}$ has to be taken into consideration in the calculation.

• Frequency of vibration

Higher frequencies increase the torsional stiffness.

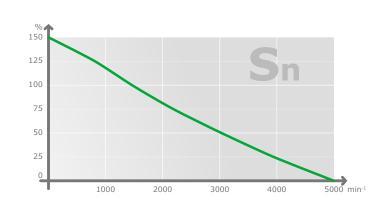
By experience the dynamic torsional stiffness is 30% higher than the static stiffness. CENTA keeps record of exact parameters.

• Amplitude of vibratory torque

Higher amplitudes reduce the torsional stiffness, therefore small amplitudes result in higher dynamic stiffness. CENTA keeps record of exact parameters.

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EXPLANATION OF THE TECHNICAL DATA



	11		12		13		14	15		
	Axial stiffness		Permissible radial displacement		Radial stiffness		rmissible angular displacement	Angular stiffness		
	[kN/mm]		[mm]		[kN/mm]		[≯°]		[kNm/°]	
Ca	The axial stiffness determines the axial reaction force on the input and output sides upon axial displacement.	ΔKr	The continuous permissible ra- dial displacement depends on the operation speed and may re- quire adjustment (see diagrams Sn of the coupling series).	Cr	The radial stiffness determines the radial reaction force on the input and output sides upon ra- dial displacement.	ΔKw	The continuous permissible an- gular displacement of the cou- pling. This is the sum of displacement by assembly as well as static and dynamic displacements dur- ing operation. The continuous permissible an- gular displacement depends on the operation speed and may re- quire adjustment (see diagrams S₀ of the coupling series).	Cw	The angular stiffness determines the restoring bending moment on the input and output sides upon angular displacement.	
Ca dyn	By experience the dynamic stiff- ness is higher than the static one. The factor depends on the coupling series.			Crdyn	By experience the dynamic stiff- ness is higher than the static one. The factor depends on the coupling series.			Cwdyn	By experience the dynamic stiff- ness is higher than the static one. The factor depends on the coupling series.	
		∆Kr ma	The maximum radial displace- ment of the coupling, which may occur occasionally and for a short period without considera- tion of the operation speed (e.g. extreme overload). ⁵ The concurrent occurrence of different kinds of displacements is handled in technical docu- ments (displacement diagrams, data sheets, assembly instruc- tions).			∆Kwma	The maximum angular displace- ment of the coupling, which may occur occasionally and for a short period without considera- tion of the operation speed (e.g. extreme overload)			

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1. This catalog supersedes previous editions.

This catalog shows the extent of our coupling range at the time of printing. This program is still being extended with further sizes and series. Any changes due to technological progress are reserved.

We reserve the right to amend any dimensions or detail specified or illustrated in this publication without notice and without incurring any obligation to provide such modification to such couplings previously delivered. Please ask for an application drawing and current data before making a detailed coupling selection.

2. We would like to draw your attention to the need of preventing accidents or injury. No safety guards are included in our supply.

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4. Torsional responsibility

The responsibility for ensuring the torsional vibration compatibility of the complete drive train, rests with the final assembler. As a component supplier CENTA is not responsible for such calculations, and cannot accept any liability for gear noise/-damage or coupling damage caused by torsional vibrations.

CENTA recommends that a torsional vibration analysis (TVA) is carried out on the complete drive train prior to start up of the machinery. In general torsional vibration analysis can be undertaken by engine manufacturers, consultants or classicfication societies. CENTA can assist with such calculations using broad experience in coupling applications and torsional vibration analysis.

- 5. Copyright to this technical dokument is held by CENTA Antriebe Kirschey GmbH.
- 6. The dimensions on the flywheel side of the couplings are based on the specifications given by the purchaser. The responsibility for ensuring dimensional compatibility rests with the assembler of the drive train. CENTA cannot accept liability for interference between the coupling and the flywheel or gearbox or for damage caused by such interference.
- 7. All technical data in this catalog are according to the metric SI system. All dimensions are in mm. All hub dimensions (N, Ni and N2) may vary, depending on the required finished bore. All dimensions for masses (m), inertias (J) and centres of gravity (S) refer to the maximum bore diameter.



HEAD OFFICE

CENTA Antriebe Kirschey GmbH



Bergische Strasse 7 42781 Haan/Germany +49-2129-912-0 Phone +49-2129-2790 Fax info@centa.de www.centa.info CENTA is the leading producer of flexible couplings for rail, industrial, marine and power generating applications. Worldwide.

WWW.CENTA.INFO/CONTACT